



# **Radiative Heat Transfer Modelling in PHOENICS**



# Why Model Radiation?

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- Some typical reasons...
- Warm surfaces in buildings will radiate heat to cooler surfaces.
- If you stand near the sun-warmed wall of a building you will feel hot.
- Many comfort indices involve a radiant temperature – we need to know what this is.
- In a fire or in a combustor, the hot smoky gases emit and absorb radiation – this affects the temperature distributions.
- Many other examples.



# Difficulty of Modelling Radiation

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- Radiation travels in straight lines.
- It is not convected or diffused.
- Therefore obeys entirely different equations from those solved in CFD.
- Accurate tracking of radiation in a model is seriously expensive!
- Spalding recognised the need for engineers to get an adequate solution within reasonable computing time.
- This led to the development of the **IMMERSOL** radiation model.



# “Optically Thin” and “Optically Thick”

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- Compare the “mean free path” of the radiation with typical distance between the radiating walls.
- **Large mean free path - “optically thin”.**  
Radiation travels long distances without being absorbed.
- Typical example - ventilation in internal spaces.
- **Small mean free path path - “optically thick”.**  
Radiation quickly absorbed - re-emitted - re-absorbed - etc.
- Typical example – hot smoky gases in fires, combustors.



# Radiosity and Radiant Temperature

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- We need to consider the meanings of these quantities.
- Consider a small volume. The **radiosity**  $R$  ( $\text{W}/\text{m}^2$ ) is defined as the sum all radiation fluxes traversing the volume.
- Imagine a small “black-body” probe inserted into the space, in thermal equilibrium with the local radiation.
- Define the temperature of such a probe as the local **radiant temperature**  $T_3$  ( $^\circ\text{K}$ ).
- $R$  and  $T_3$  are related by the equation:  
$$R = \sigma (T_3)^4$$
- $\sigma$  is the Stefan-Boltzmann constant =  $5.67\text{E}8 \text{ W m}^{-2} \text{ K}^{-4}$
- **The IMMERSOL model solves for  $T_3$ .**



# Equation for Radiant Temperature

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- In the **thick optical limit** (e.g. thick smoke) radiant temperature obeys a conduction-type equation.
- Wall temperatures form the boundary condition.
- Can be shown that the resistivity (i.e. temperature gradient / radiation flux) is  $(3/16) (e+s) / \sigma T^3$ .
- Note e, s are the emissivity, scattering coeffs per unit length
- In the **thin optical limit** (clear air) we ASSUME that radiant temperature obeys a similar equation.
- This is the big assumption of IMMERSOL.
- Given this, it is easy to show that the resistivity is  $(0.25 / w_{\text{gap}}) / \sigma T^3$
- (Note  $w_{\text{gap}}$  is the distance between the hot and cold walls.)
- (Note this also assumes the temperature difference is small.)



# Equation for Radiant Temperature

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- IMMERSOL has to cover both optically thin and thick, and intermediate states.
- We ASSUME (1) that T3 obeys a conduction-type equation (as discussed above) for the general case,
- ASSUME (2) a general approach can be obtained by adding the resistivities for thin and thick scenarios:
- Resistivity is  $((3/16) (e+s) + 0.25 / w_{\text{gap}}) / (\sigma T^3)$
- Note for optically thin case (e+s) is zero, so first term drops out, leaving the correct (approximate) resistivity.
- For optically thick case (e.g. smoke), emissivity per unit length is large, so first term dominates – also correct.



# Equation for Radiant Temperature

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- So, to summarise:
- **IMMERSOL** solves a conduction equation for  $T_3$  with the above resistivity, for given boundary wall temperatures.
- $T_3$  can be used to establish:
  - wall surface temperatures via a surface heat balance,
  - comfort indices for wind or ventilation cases,
  - amount of radiative heating for smoke or combustion cases.
- Details of the derivation are in the POLIS article on Immersol.





# Boundary Conditions

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- We have seen that the T3 equation is a conduction-type equation. There is no convection of T3.
- The boundary conditions for T3 are the wall temperatures.
- At some boundaries, the wall temperature may be specified.
- At others, the wall temperature is determined by solving a surface heat balance equation at the wall.
- Thermal radiation to/from the wall, heat convection at the surface, and heat conduction away from the surface, must all balance.
- The wall temperature derived from this balance is stored in the variable **TWAL** which can be plotted.



# Flow Boundaries

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- At **inflow or outflow boundaries** need to specify whether radiation can pass through...
- And if so, what is the external temperature that the radiation “sees” through the boundary.
- This is set in the Attributes panel:

External Radiative Link  Yes

T external   °C

- In a **Wind model** with temperature and radiation (e.g. Urban Heat Island) this appears in the Wind attributes.
- Need to say “Yes” and give suitable “**Sky temperature**”.
- E.g. “Survey of Sky Effective Temperature Models Applicable to Building Envelope Radiant Heat Transfer” by Algarni and Nutter.
- July 2015 / DOI:[10.13140/RG.2.1.4212.5526](https://doi.org/10.13140/RG.2.1.4212.5526) / Report number: AT-15-029



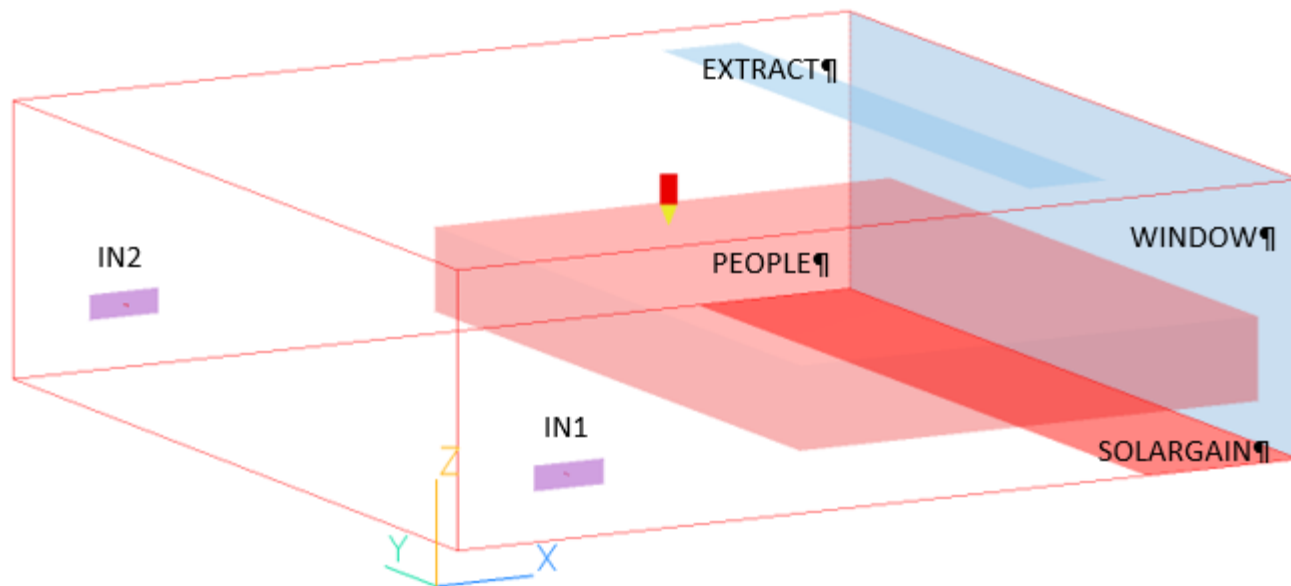
# Example – Ventilation and Natural Convection in a Room

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3 heat sources:

- people (the pink box),
- solar gain (on the floor near the window),
- window (with high external temperature).

surface emissivities = 1



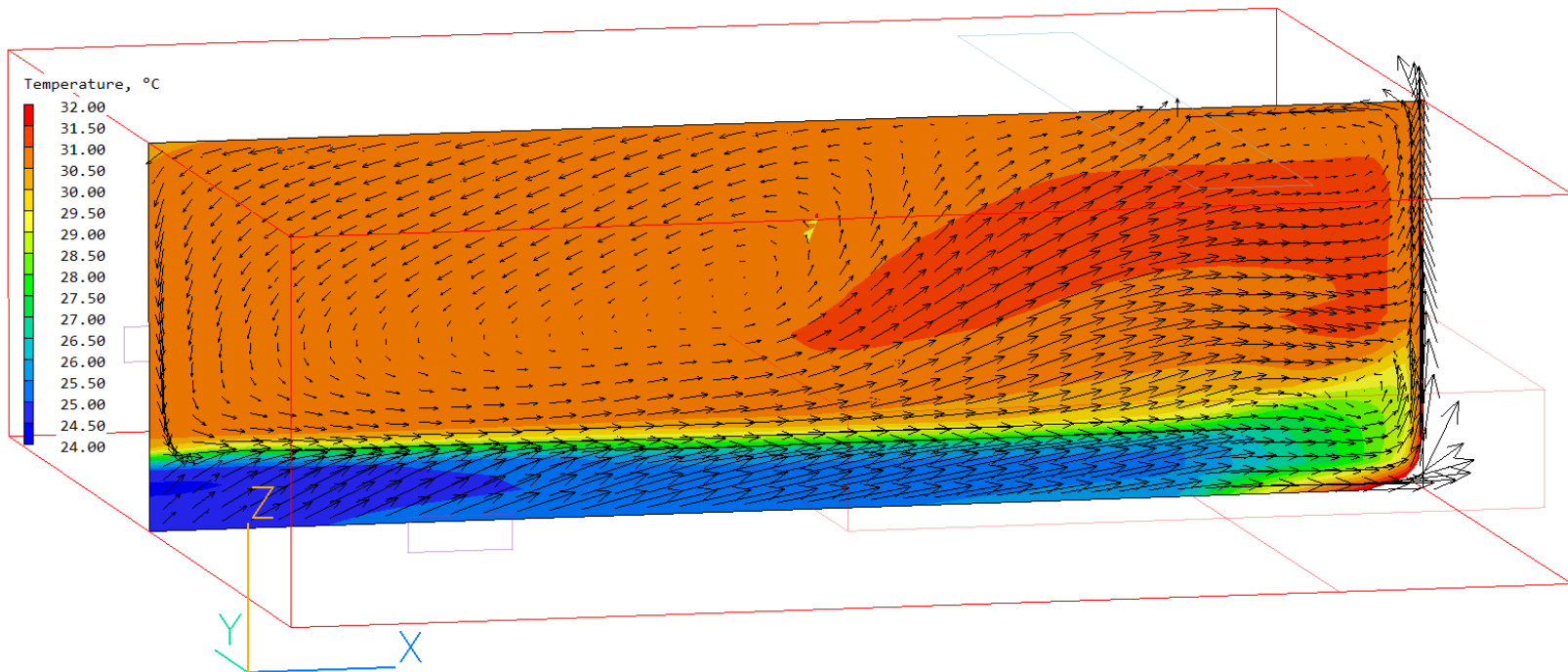
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# Example – Ventilation and Natural Convection in a Room

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- Contours of temperature TEM1



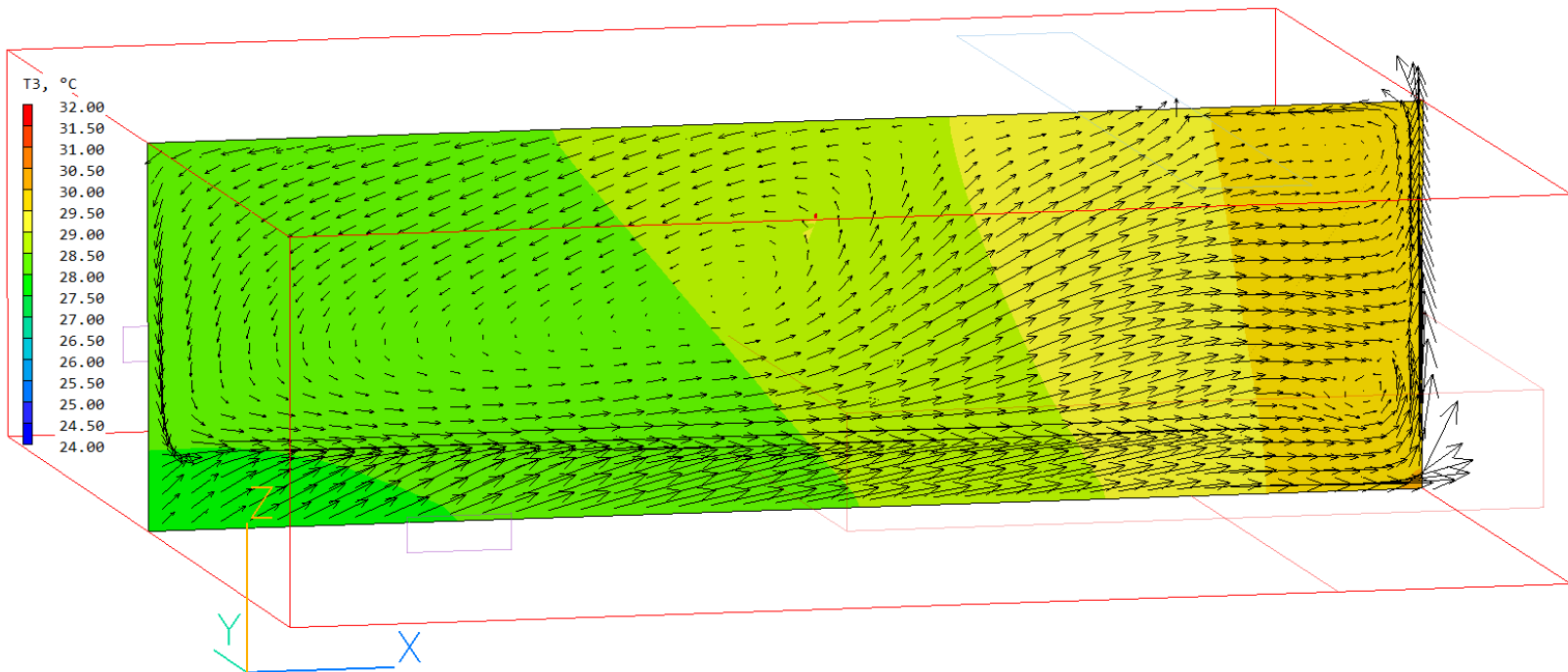
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# Example – Ventilation and Natural Convection in a Room

Lecture

- Contours of temperature T3



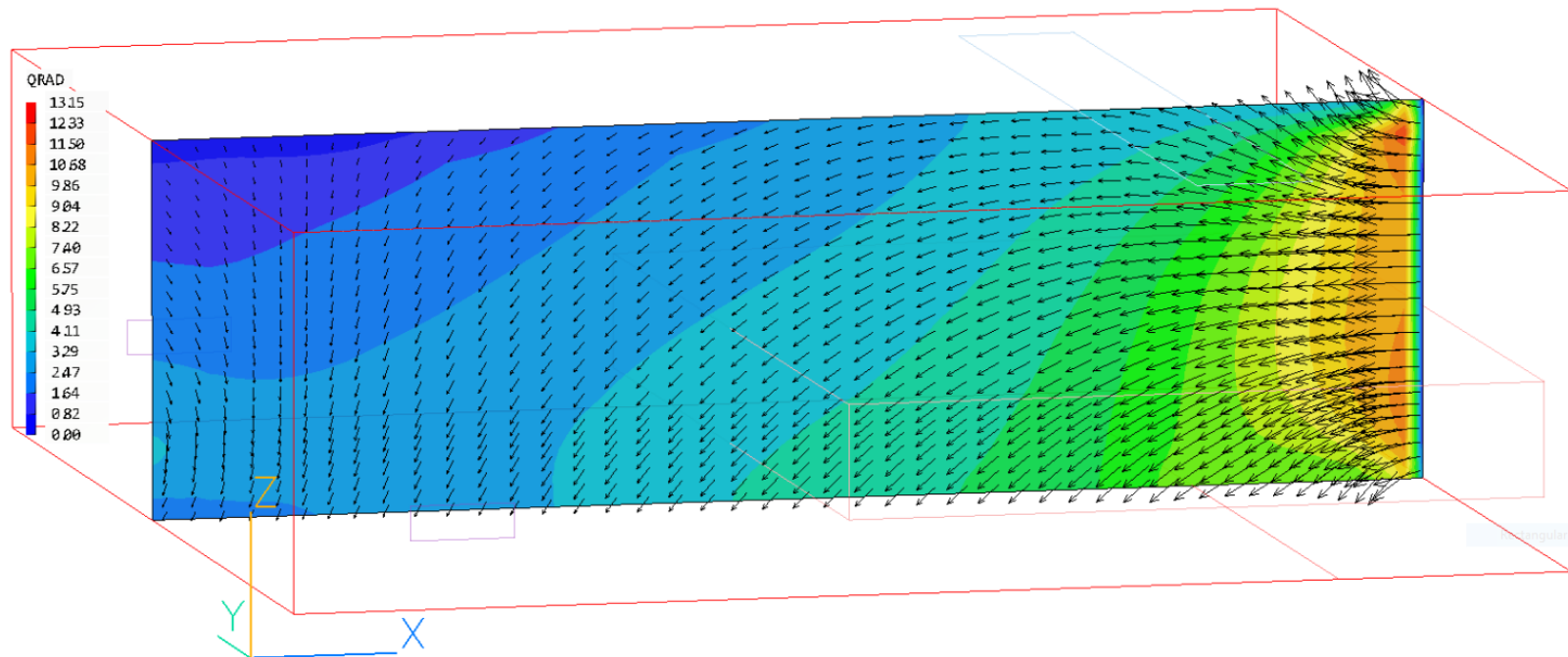
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# Example – Ventilation and Natural Convection in a Room

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- Contours of Radiation Flux Intensity
- Vectors of Radiation Flux



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# Energy Source Term

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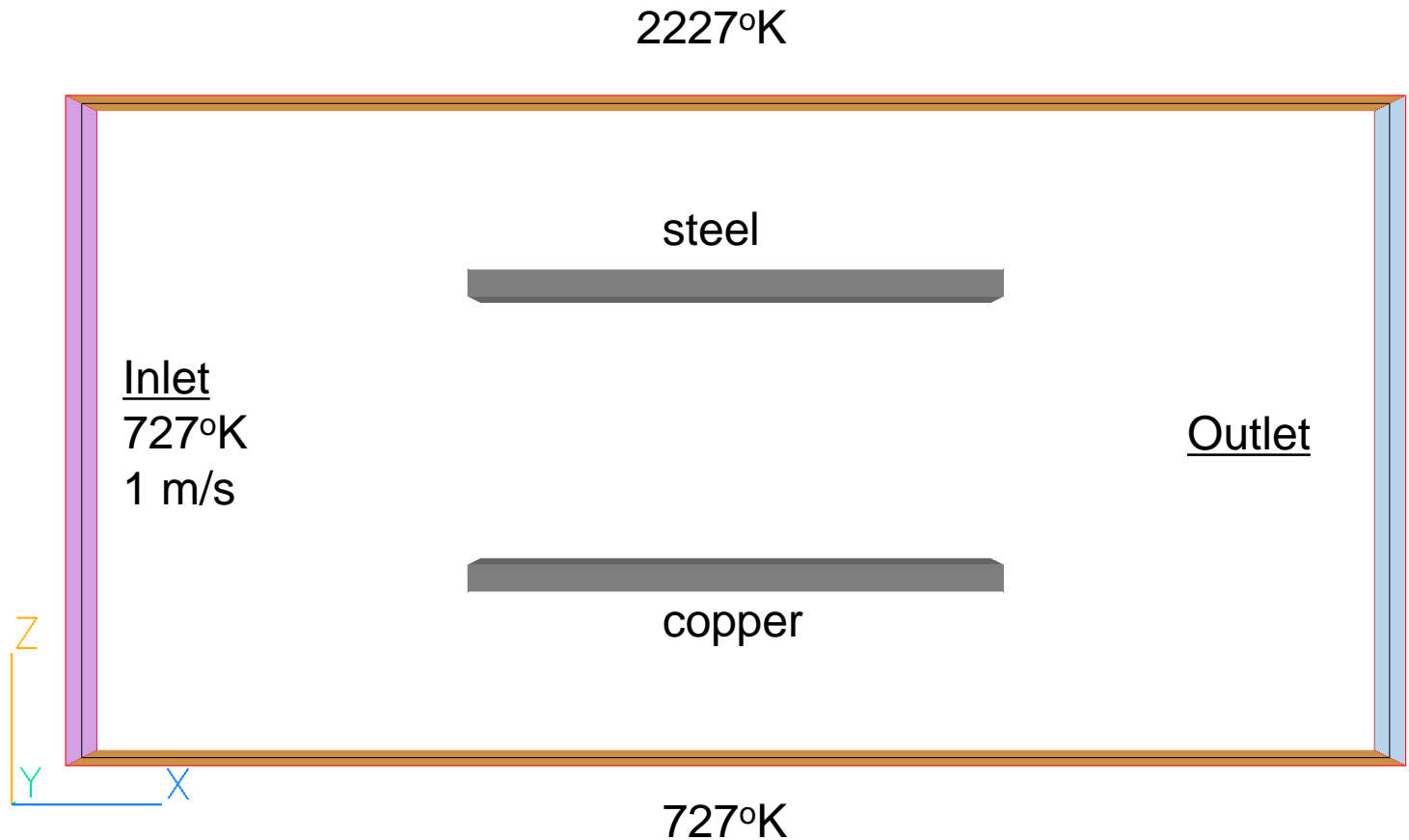
- The **energy equation (TEM1)** contains a **source term** corresponding to radiation absorbed/emitted by the gas (for optically thick cases).
- This term is proportional to  $\sigma^* (T3^4 - TEM1^4)$
- An equal and opposite source term appears in the T3 equation.
- For an optically thin medium the term is zero.
- In the RESULT file, the Nett Sources for TEM1 and T3 will not balance individually, due to this transfer of energy between T3 and TEM1.
- **An overall heat balance (for TEM1 plus T3) is also printed, and this should be close to zero.**



# Example – Duct Flow with Hot Wall

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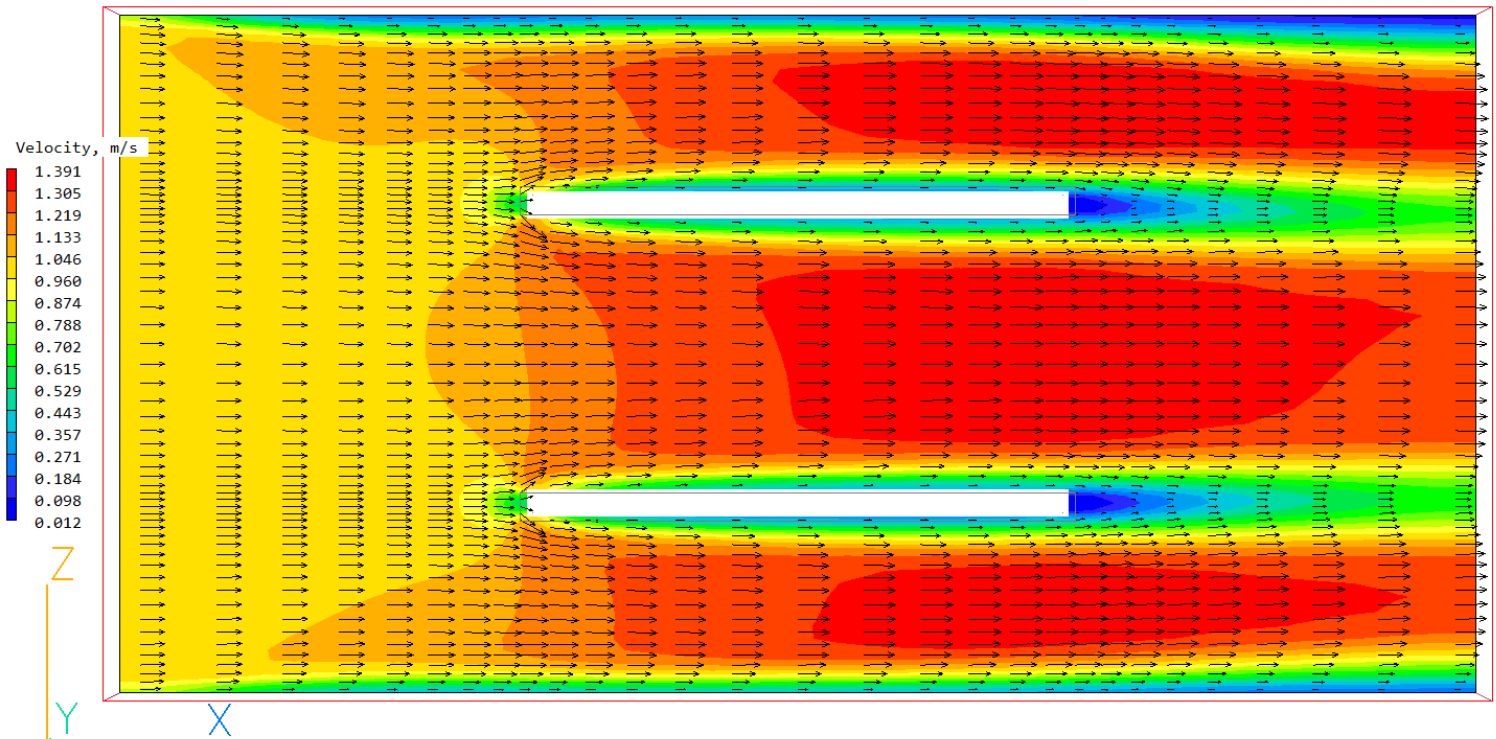




# Example – Duct Flow with Hot Wall

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- Optically thin (gas absorption coeff / unit length = 0)
- Velocity contours



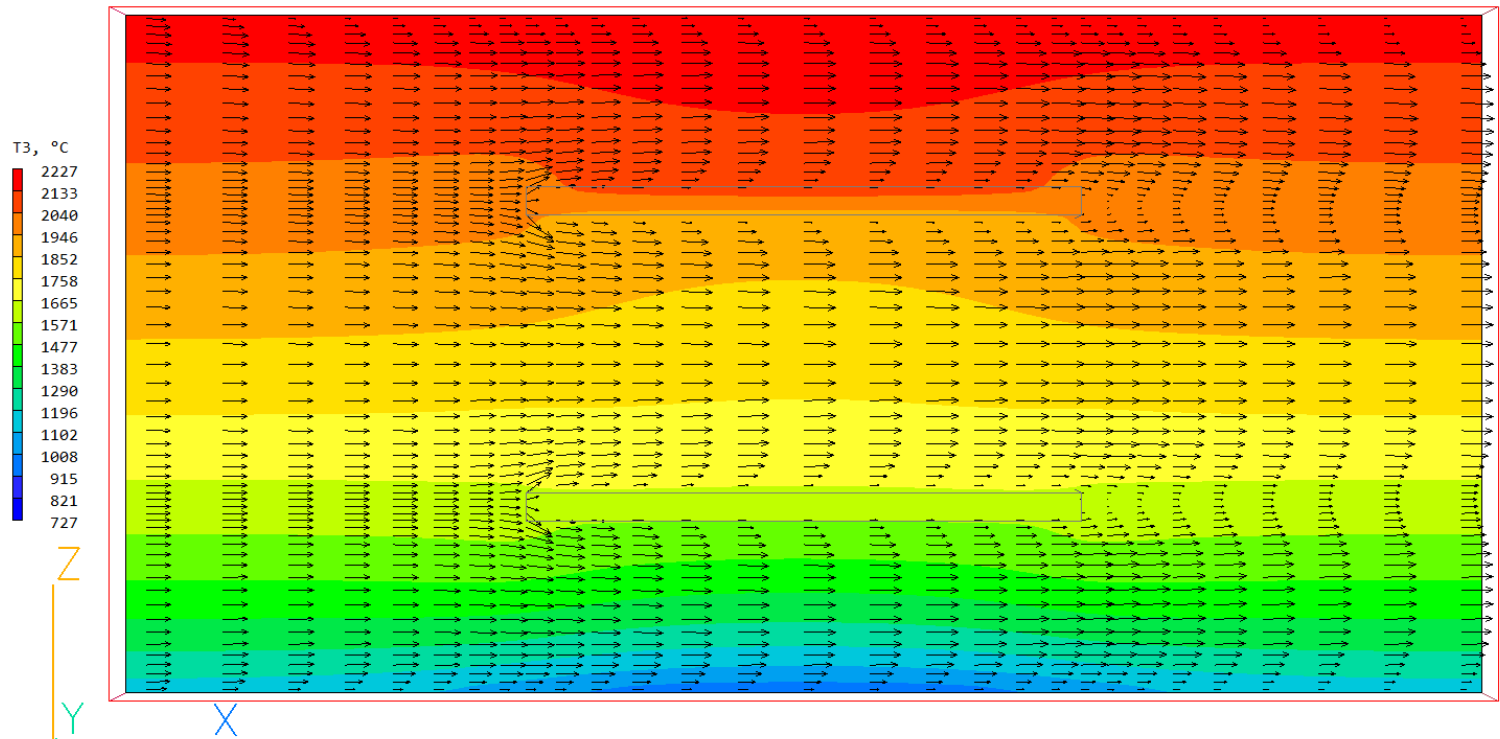
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# Example – Duct Flow with Hot Wall

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- Optically thin
- Radiant Temperature ( $T_3$ )



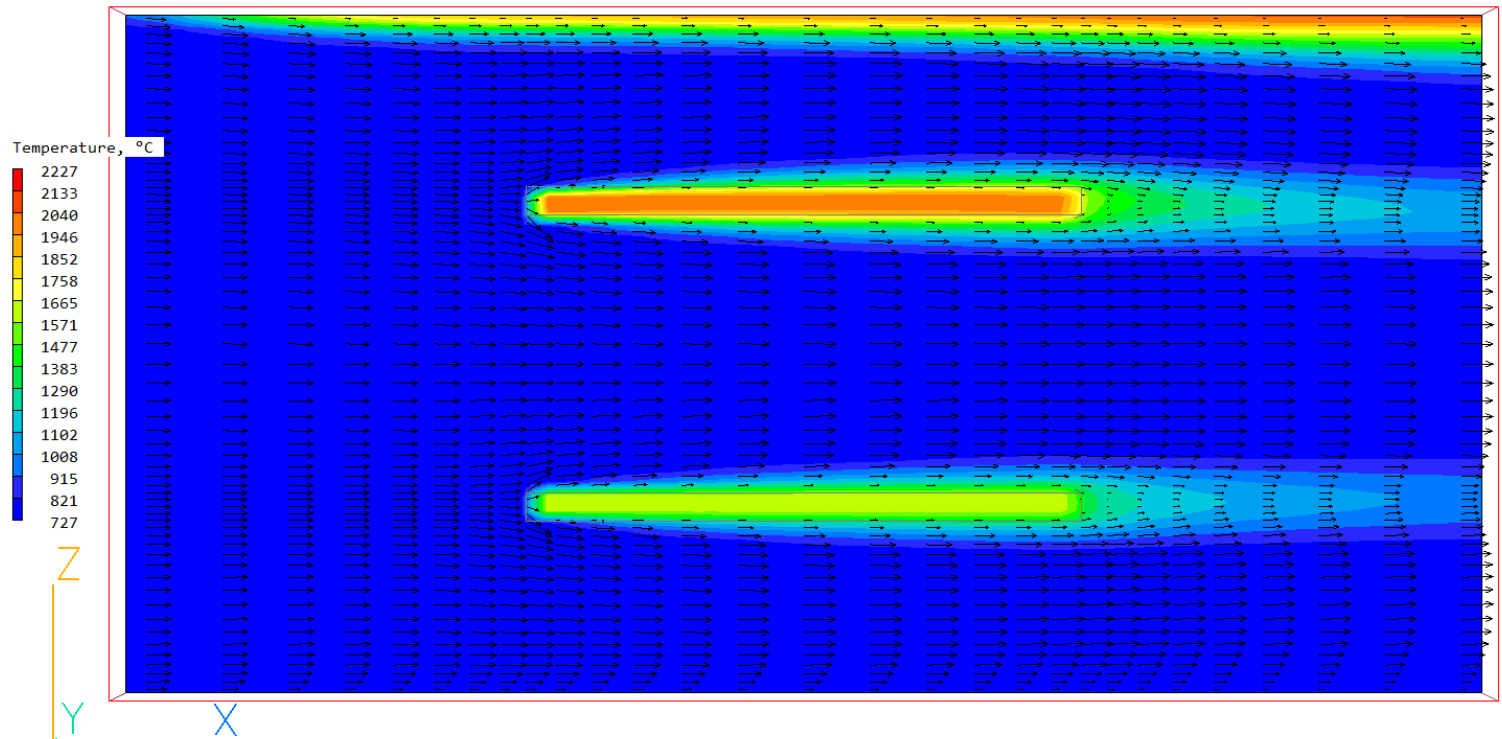
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# Example – Duct Flow with Hot Wall

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- Optically thin
- Temperature (TEM1)



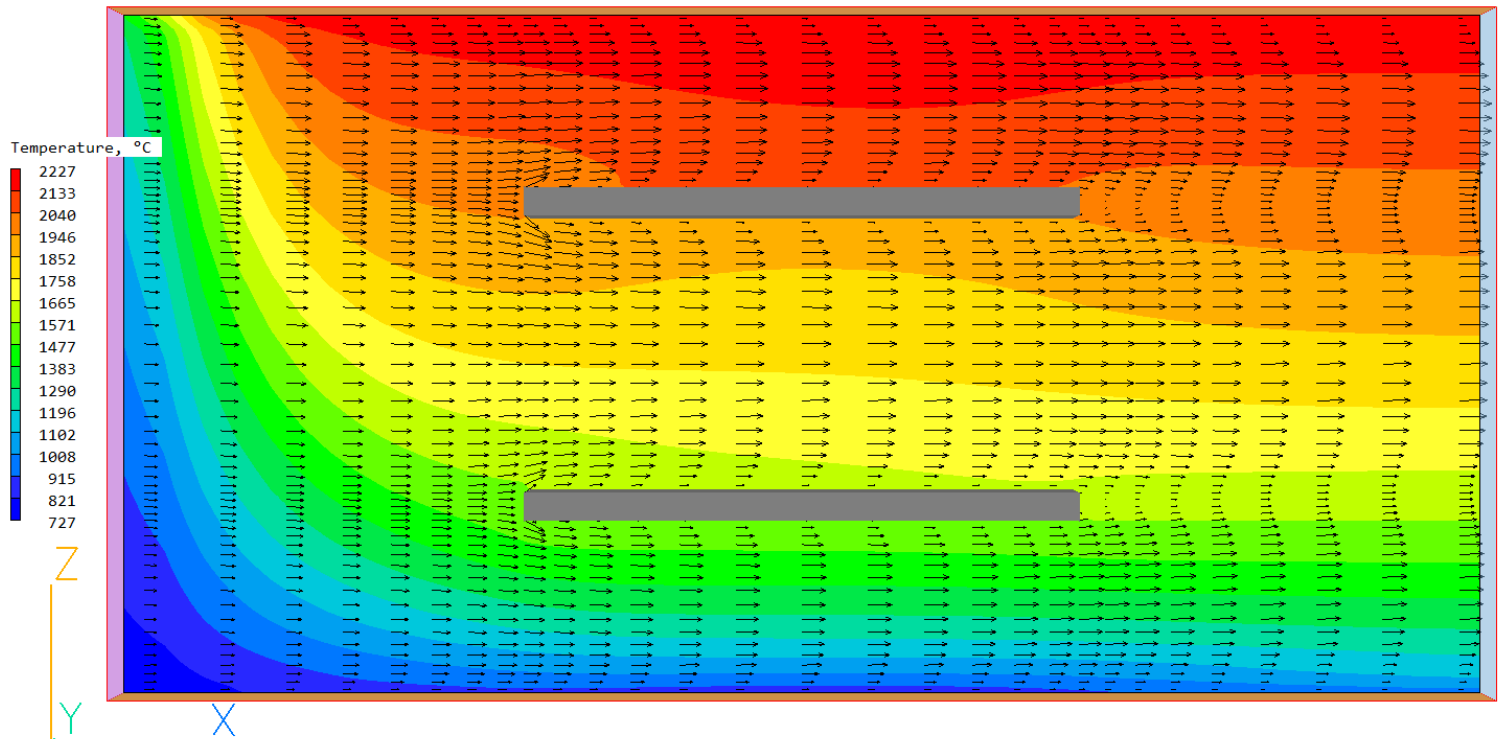
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# Example – Duct Flow with Hot Wall

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- Optically thick (absorption coeff / unit length = 1)
- Temperature (TEM1)



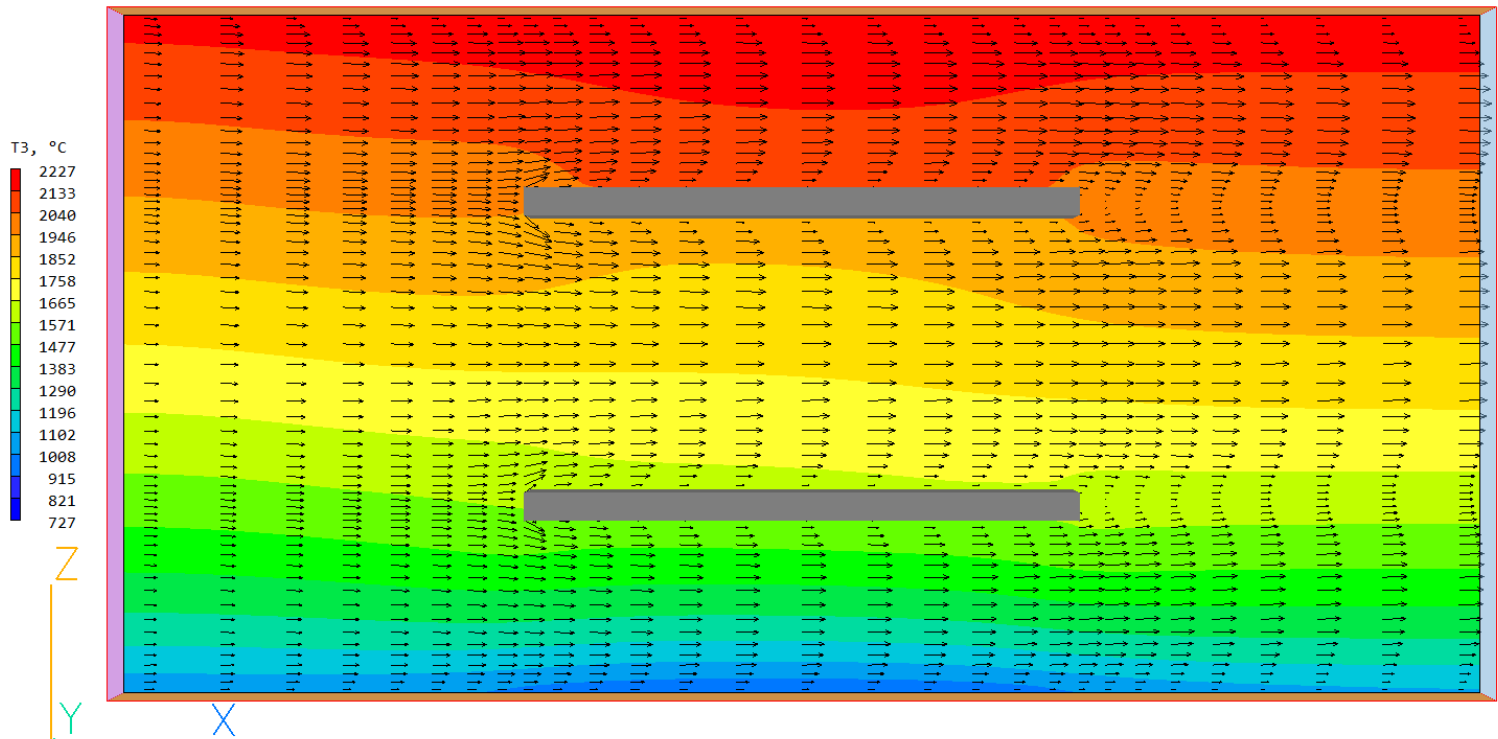
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# Example – Duct Flow with Hot Wall

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- Optically thick
- Radiant Temperature ( $T_3$ )



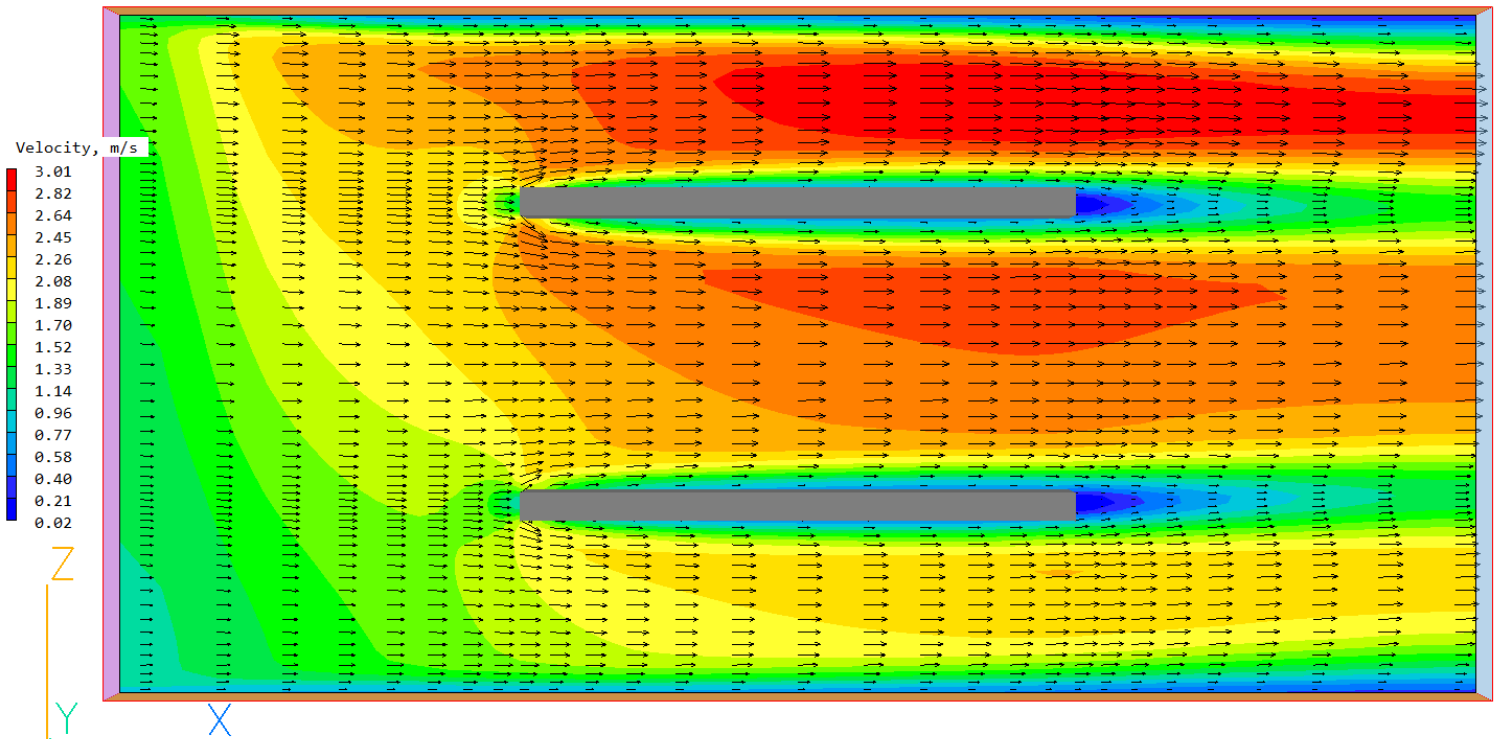
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# Example – Duct Flow with Hot Wall

Lecture

- Optically thick
- Velocity contours



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# Relaxation for T3

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- For optically thin cases, setting Linear relaxation with amount 0.25 should be fine.
- For optically thick cases, either try the above, or use the same relaxation settings as for TEM1.

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# IMMERSOL and Wavelength

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## Two important points

- The PHOENICS implementation of IMMERSOL has no wavelength dependence.
- Solar radiation (short wavelength) is NOT modelled in IMMERSOL.

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# IMMERSOL and Solar Radiation

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- The SUN object in FLAIR creates **heat sources** where the sun shines on solids.
- **We do not model the solar radiation that creates these heat sources.**
- Some of this heat is re-radiated (long wavelength).
- **It is this long-wave infra-red radiation that is handled by IMMERSOL.**
- An example follows – but we discuss Comfort Indices first.



# Radiation Modelling and Comfort Indices

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- Comfort indices measure degree of comfort, e.g.:
- **Universal Thermal Climate Index (UTCI)**  
UTCI is a function of air temperature, water vapour pressure, **radiant temperature** and wind speed
- **Predicted Mean Vote (PMV)**  
PMV measures comfort, based on air temp, water vapour pressure, **radiant temp**, wind speed, and various parameters measuring human metabolic rate and heat transfer
- **These indices use the radiant temperature  $T_3$  ...**
- **... which can be determined by using IMMERSOL**



# Radiation Modelling and Comfort Indices

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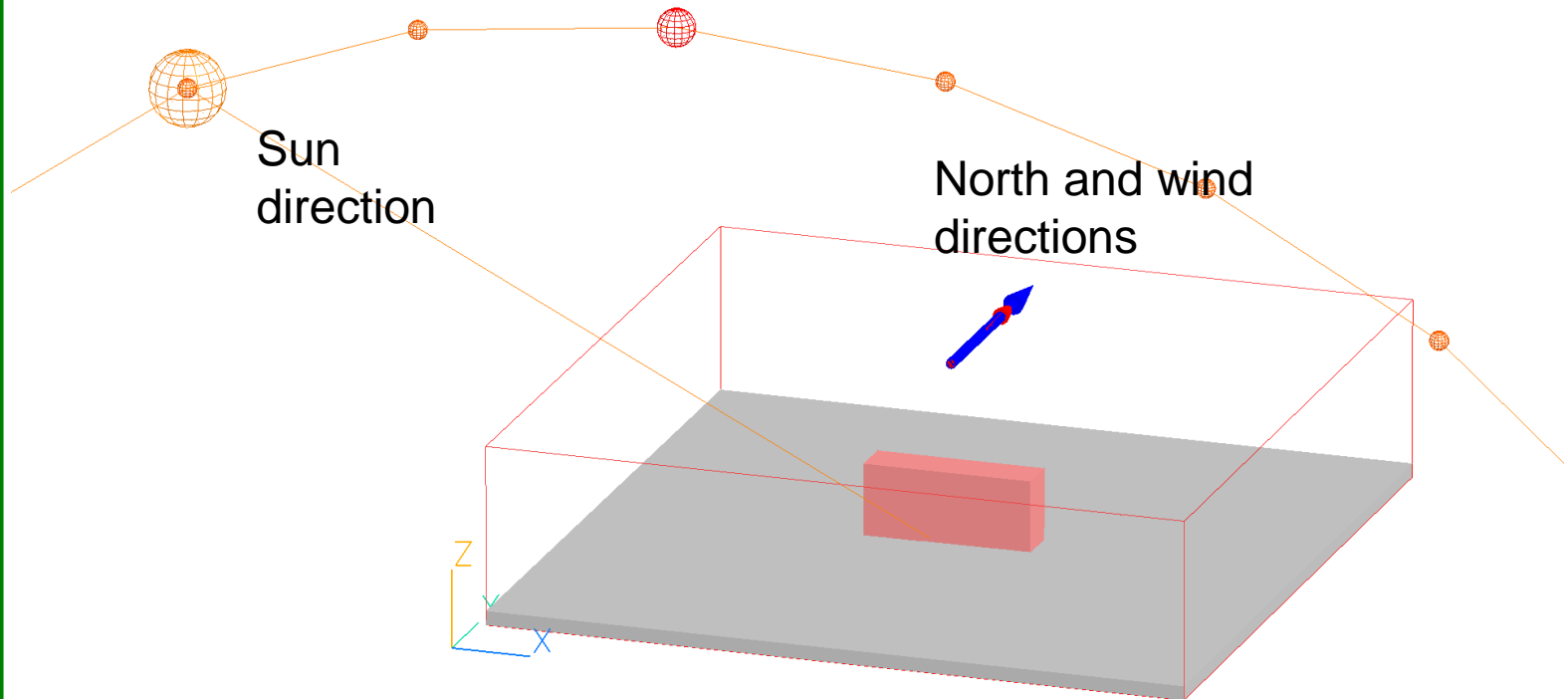
- Note: The comfort indices also use water vapour pressure.
- This can be determined by solving for humidity in FLAIR.



# Example – Building in the Sun

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- Wind 5 m/s from S, 20°C
- RH 65%
- Building 120 x 30 x 51m
- Latitude of Hong Kong
- 21 December, 2.00 p.m.
- Sky temperature 0°C
- Contour plots 1.75m above ground



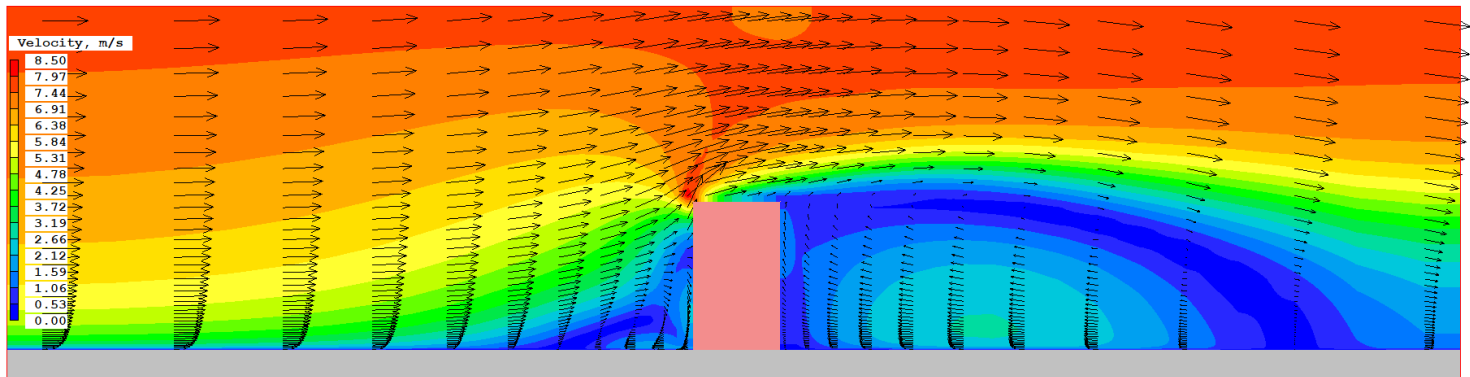
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# Example – Building in the Sun

Lecture

- Velocities in vertical plane
- Note the recirculation behind the building



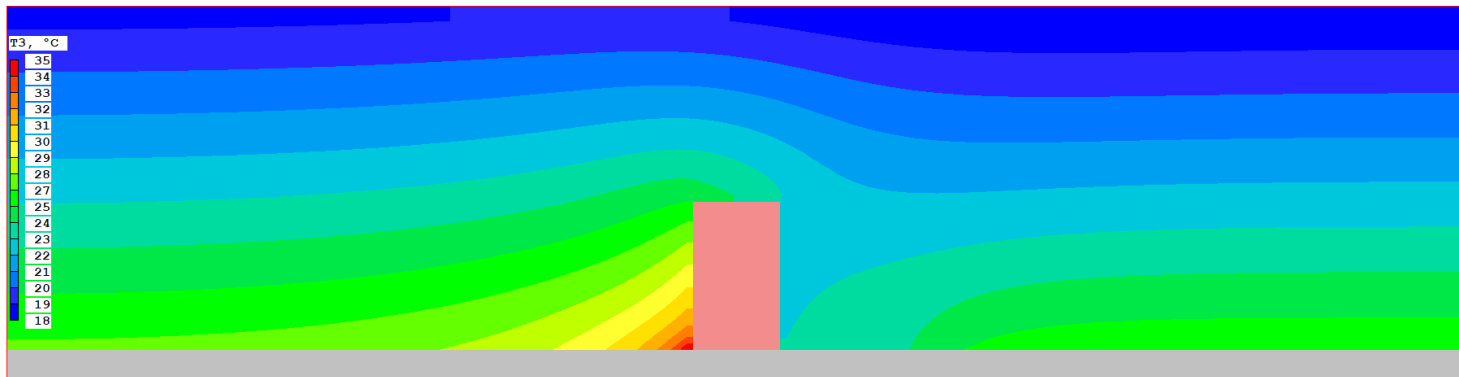
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# Example – Building in the Sun

Lecture

- Radiant Temperature ( $T_3$ )
- If you stand in front of the sunlit building it feels warm



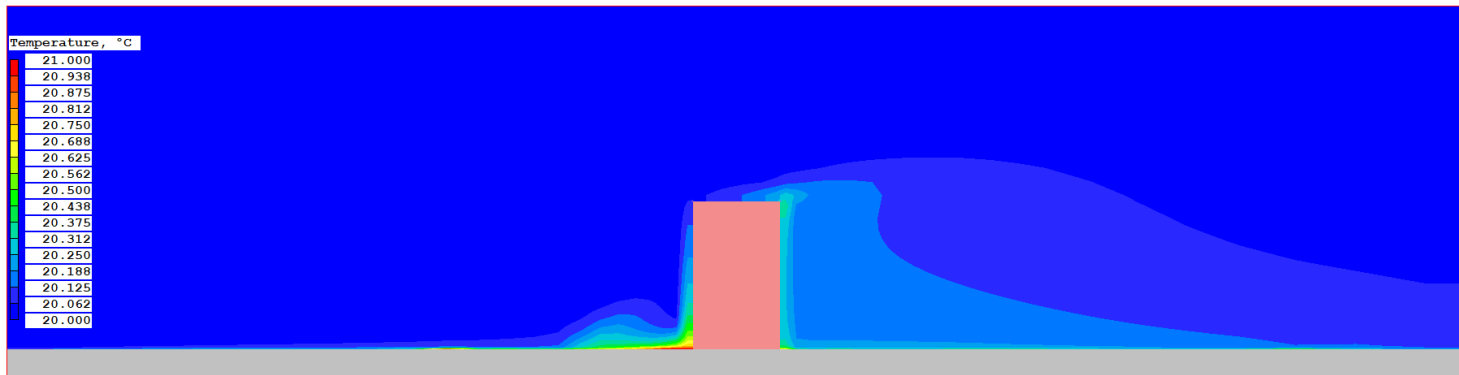
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# Example – Building in the Sun

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- Temperature (TEM1)
- The actual temperature varies by less than 1°, and only very close to the solid surfaces



- Observe how T3 is completely different from TEM1

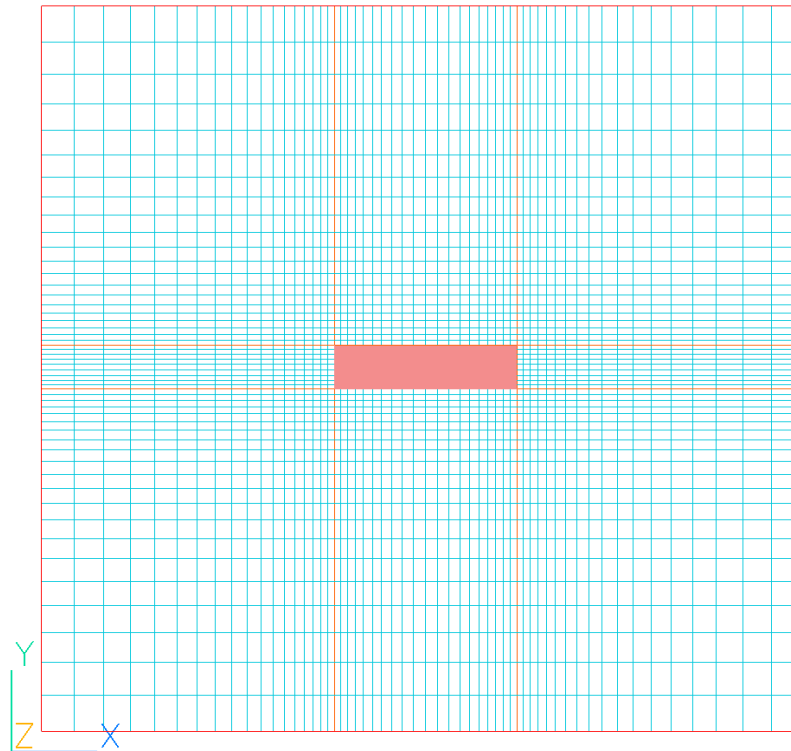
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# Example – Building in the Sun

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- Mesh in horizontal plane



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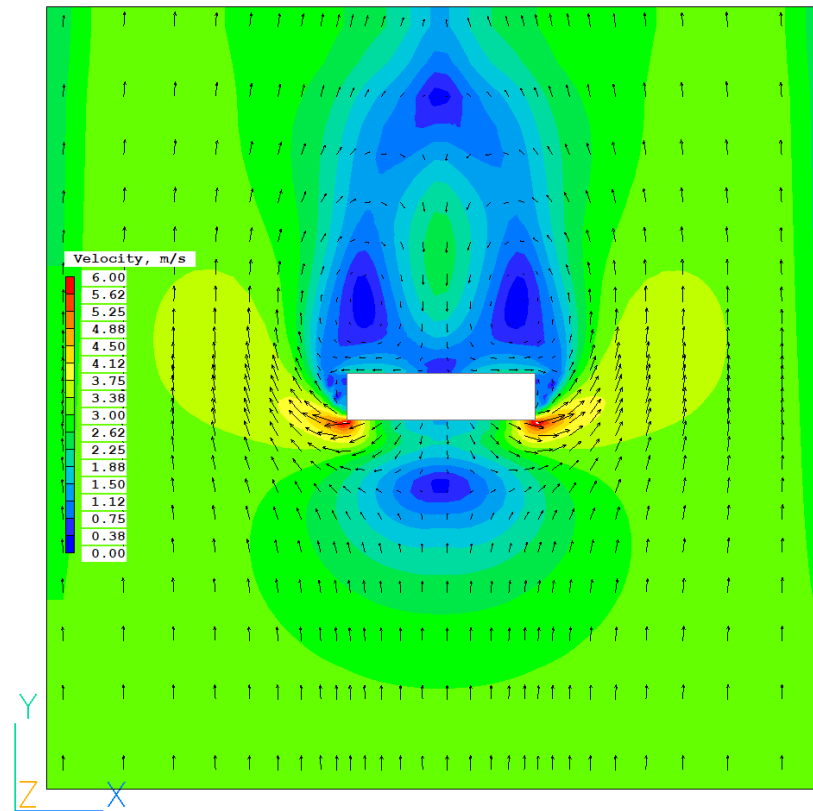




# Example – Building in the Sun

Lecture

- Velocities in horizontal plane 1.75 m from the ground



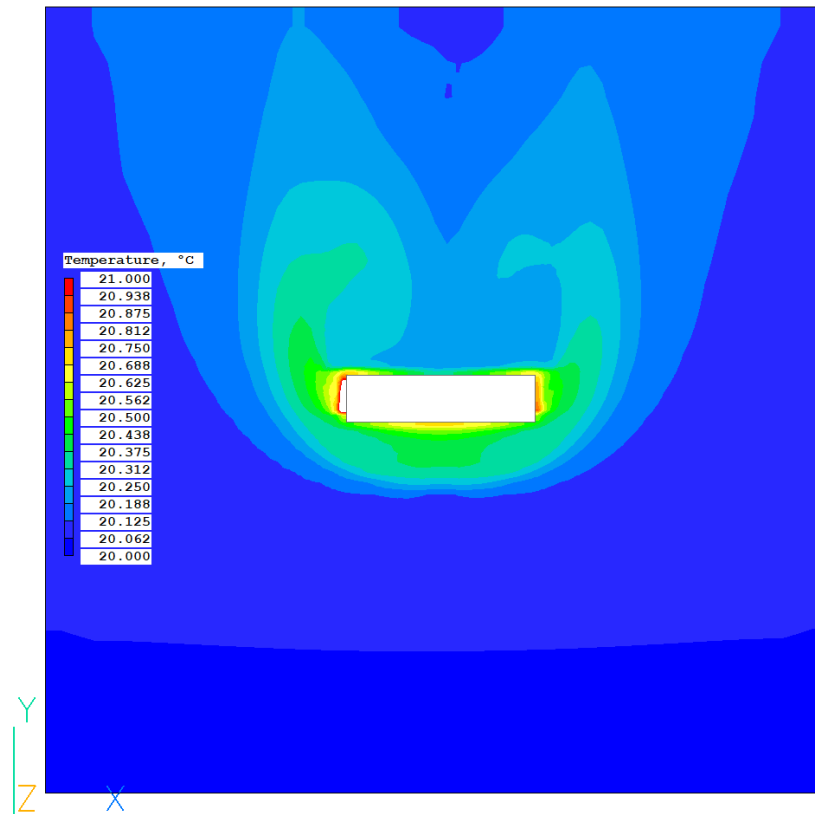
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# Example – Building in the Sun

Lecture

- Temperature (TEM1)



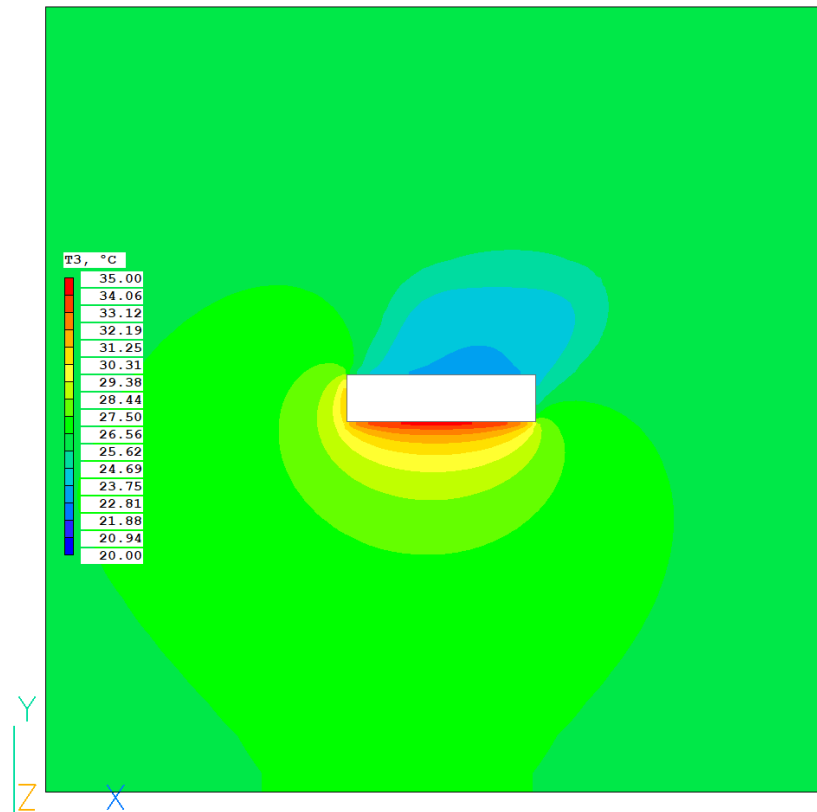
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# Example – Building in the Sun

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- Radiant Temperature (T3)
- It will feel hot in front of the building



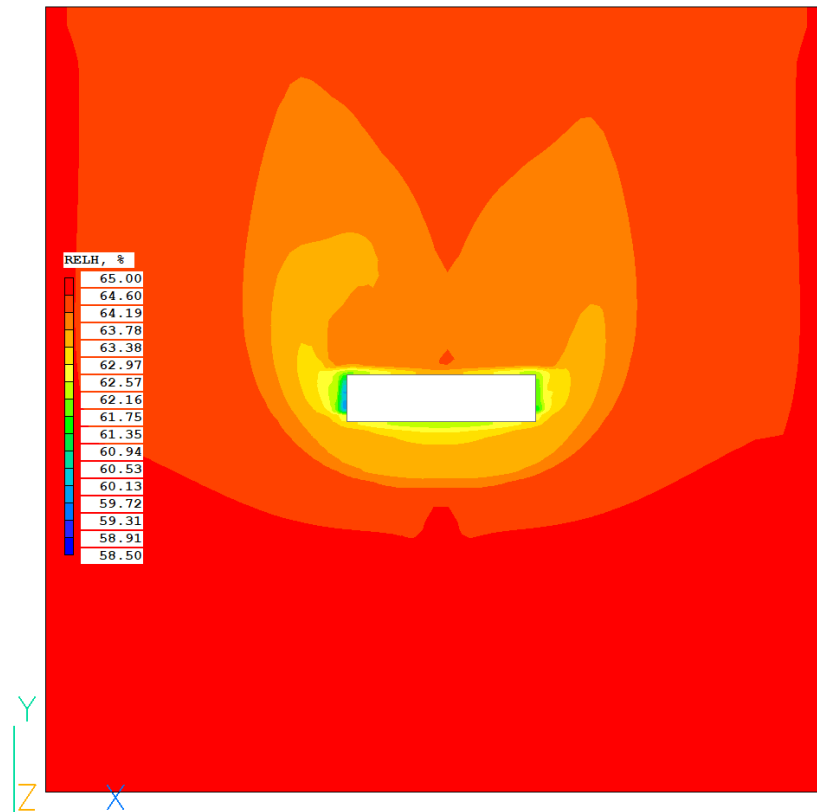
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# Example – Building in the Sun

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- Relative Humidity
- (Required for the comfort indices)



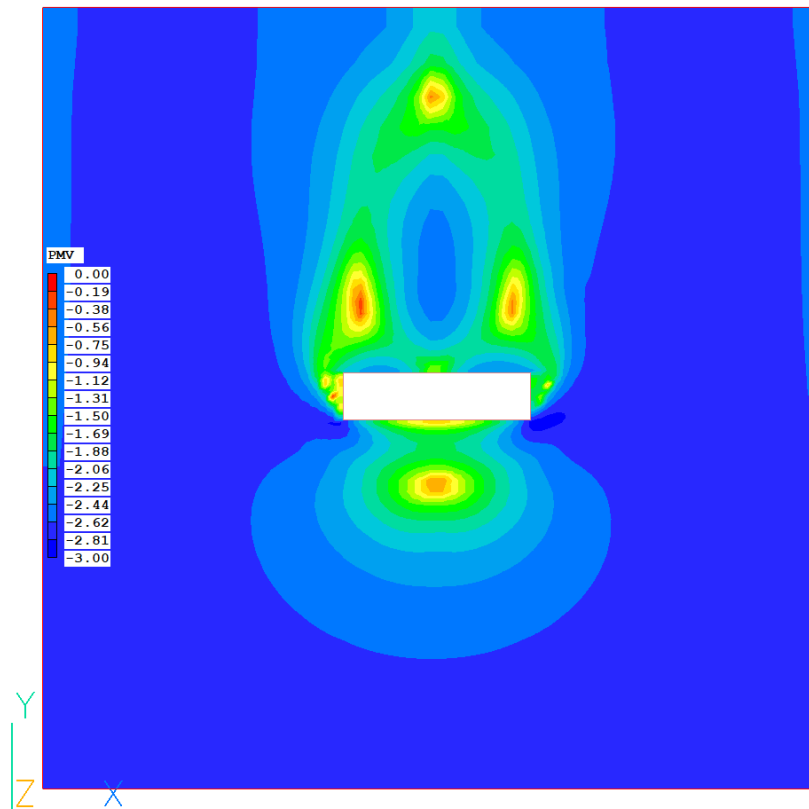
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# Example – Building in the Sun

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- Predicted Mean Vote (PMV)
- (0 feels “neutral”, -3 feels “cold”)



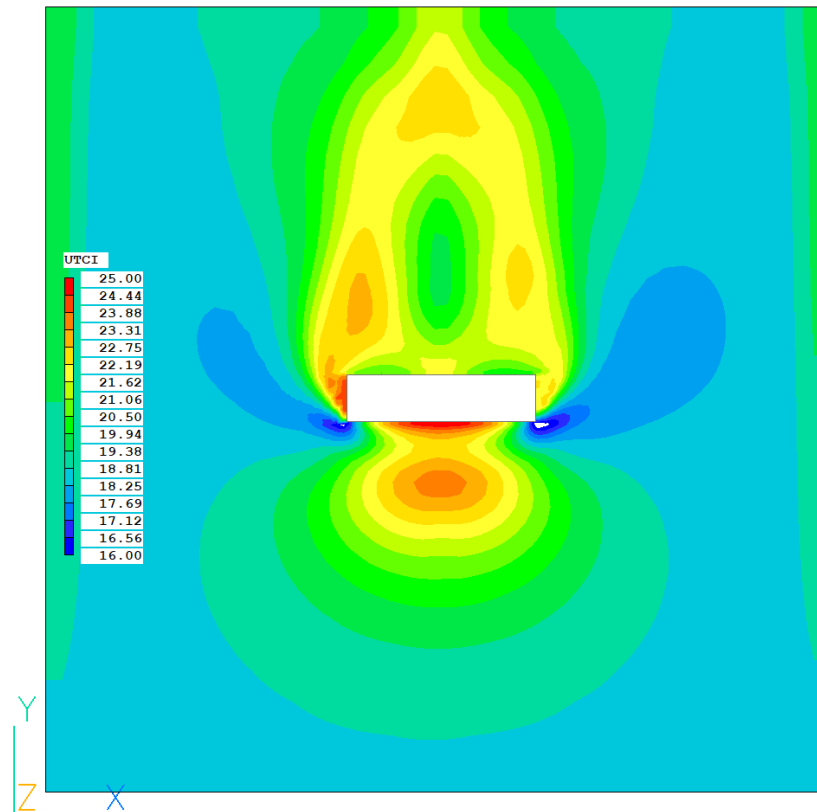
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# Example – Building in the Sun

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- Universal Thermal Comfort Index (UTCI)



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## Some Final Remarks...

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- IMMERSOL is activated from the “Models” Menu, via the “Radiation Models” button.
- The “Settings” button allows the **absorption and scattering coefficients** (per unit length) to be set.
- For a transparent medium, both should be zero.
- In fire simulations, the **gas emissivity** is often a function of smoke concentration (this requires InForm).
- Note – “absorptivity” and “emissivity” are basically the same.
- The “Settings” button also allows storage of the **radiative heat fluxes** in each direction. These can then be plotted as vectors in the Viewer.



## Some Final Remarks...

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- Before starting a run using IMMERSOL, check that:
  - You have set relaxation for T3 appropriately (see above).
  - All internal surfaces have sensible emissivities. The default value is 1. A suitable value for many materials is 0.9.
  - Inlets or outlets which allow radiation to pass through have “External radiative link” set.
- Remember to check the overall energy balance for TEM1 and T3 in the Result file – this appears just below the Nett Sources printout.





## Some Final Remarks...

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- IMMERSOL is the only radiation model to combine universal applicability with economic practicability for complex geometries.
- We have seen that IMMERSOL involves significant assumptions - the solutions are not exact.
- But wherever tested it has performed well, in respect of:
  - accuracy, where exact solutions are known;
  - plausibility, where they are not;
  - economy, in all circumstances.

\*\*\* THE END \*\*\*